

# Lecture 24

**Chemical Reaction Engineering** (CRE) is the field that studies the rates and mechanisms of chemical reactions and the design of the reactors in which they take place.

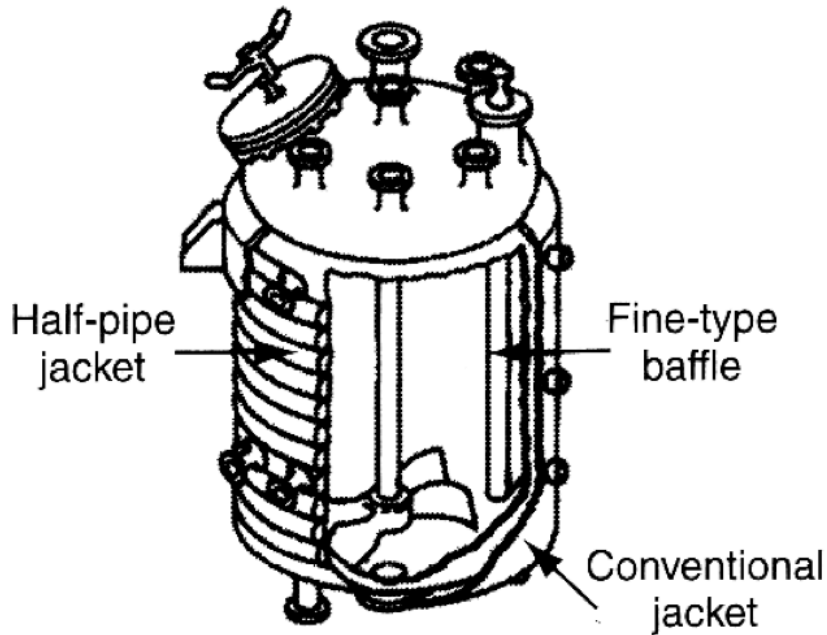
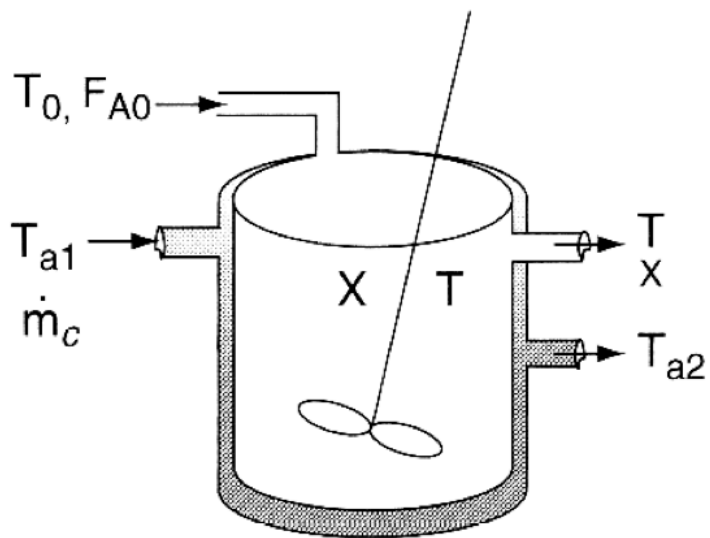
# Web Lecture 24

Class Lecture 20 - Tuesday 3/26/2013

## CSTR With Heat Effects

- Multiple Steady States
- Ignition and Extinction Temperatures

# CSTR with Heat Effects



Courtesy of Pfaudler, Inc.

# Unsteady State Energy Balance

$$\dot{Q} - \dot{W}_S + \sum_{i=1}^n F_{i0} H_{i0} - \sum_{i=1}^n F_i H_i = \frac{d\hat{E}_{\text{sys}}}{dt}$$

Neglect

Using  $\hat{E}_{\text{sys}} = \sum N_i E_i = \sum N_i (H_i - PV_i) = \sum N_i H_i - PV$

$$\frac{dE_{\text{sys}}}{dt} = \frac{d \sum N_i H_i}{dt} = \sum N_i \frac{dH_i}{dt} = \sum H_i \frac{dN_i}{dt}$$

$$\frac{dH_i}{dt} = C_{Pi} \frac{dT}{dt}$$

$$\frac{dN_i}{dt} = -\nu_i r_A V + F_{i0} - F_i$$

# Unsteady State Energy Balance

We obtain after some manipulation:

$$\frac{dT}{dt} = \frac{\dot{Q} - \dot{W}_S - \sum F_{i0} C_{Pi} (T - T_{i0}) + [-\Delta H_{RX}(T)](-r_A V)}{\sum N_i C_{Pi}}$$

Collecting terms with  $\dot{Q} = UA(T_c - T)$  and high coolant flow rates, and  $F_{i0} = F_{A0} \Theta_i$

# Unsteady State Energy Balance

$$\frac{dT}{dt} = \frac{(\Delta H_{R_X})(r_A V) - \left[ F_{A0} \overbrace{\sum \Theta_i C_{P_i}}^{C_{P_0}} (T - T_0) + (UA(T - T_a)) \right]}{\sum N_i C_{P_i}}$$

$$= \frac{F_{A0}}{\sum N_i C_{P_i}} \left[ \overbrace{\Delta H_R \frac{r_A V}{F_{A0}}}^{G(T)} - \overbrace{\left[ C_{P_0} \left[ T - T_0 + \frac{UA}{\underbrace{F_{A0} C_{P_s}}_{\kappa}} (T - T_a) \right] \right]}^{R(T)} \right]$$

# Unsteady State Energy Balance

$$\frac{dT}{dt} = \frac{F_{A0}}{\sum N_i C_{P_i}} [G(T) - R(T)]$$

$$G(T) = (r_A V) [\Delta H_{R_x}]$$

$$R(T) = C_{P_0} [(1 + \kappa)T - (T_0 + \kappa T_a)]$$

$$R(T) = C_{P_0} (1 + \kappa) \left( T - \frac{T_0 + \kappa T_a}{1 + \kappa} \right) = C_{P_0} (1 + \kappa) (T - T_C)$$

$$\kappa = \frac{UA}{F_{A0} C_{P_0}}$$

$$T_C = \frac{T_0 + \kappa T_a}{1 + \kappa}$$

# Unsteady State Energy Balance

$$\frac{dT}{dt} = G(T) - R(T)$$

If  $G(T) > R(T)$       Temperature Increases

If  $R(T) > G(T)$       Temperature Decreases



# Steady State Energy Balance for CSTRs

At Steady State

$$\frac{dT}{dt} = \frac{dN_A}{dt} = 0$$

$$-r_A V = F_{A0} X$$

$$G(T) - R(T) = 0$$

$$(-\Delta H_{RX})F_{A0} X - F_{A0} \sum \Theta_i C_{P_i} (T - T_0) - UA(T - T_a) = 0$$

Solving for X.

# Steady State Energy Balance for CSTRs

Solving for X:

$$X = \frac{\sum \Theta_i C_{P_i} (T - T_0) + \frac{UA}{F_{A0}} (T - T_a)}{-\Delta H_{Rx}^{\circ}} = X_{EB}$$

Solving for T:

$$T = \frac{F_{A0} X (-\Delta H_{Rx}) + UA T_a + F_{A0} \sum \Theta_i C_{P_i} T_0}{UA + F_{A0} \sum \Theta_i C_{P_i}}$$

## Steady State Energy Balance for CSTRs

$$X(-\Delta H_{\text{RX}}) = C_{P_0} \left[ T - T_0 + \frac{UA}{F_{A0} C_{P_0}} (T - T_a) \right]$$

$$\text{Let } \kappa = \frac{UA}{F_{A0} C_{P_0}}$$

$$\begin{aligned} X(-\Delta H_{\text{RX}}) &= C_{P_0} (T + \kappa T - T_0 - \kappa T_a) = C_{P_0} (1 + \kappa) \left( T - \frac{T_0 + \kappa T_a}{1 + \kappa} \right) \\ &= C_{P_0} (1 + \kappa) (T - T_C) \end{aligned}$$

$$T_C = \frac{T_0 + \kappa T_a}{1 + \kappa}$$

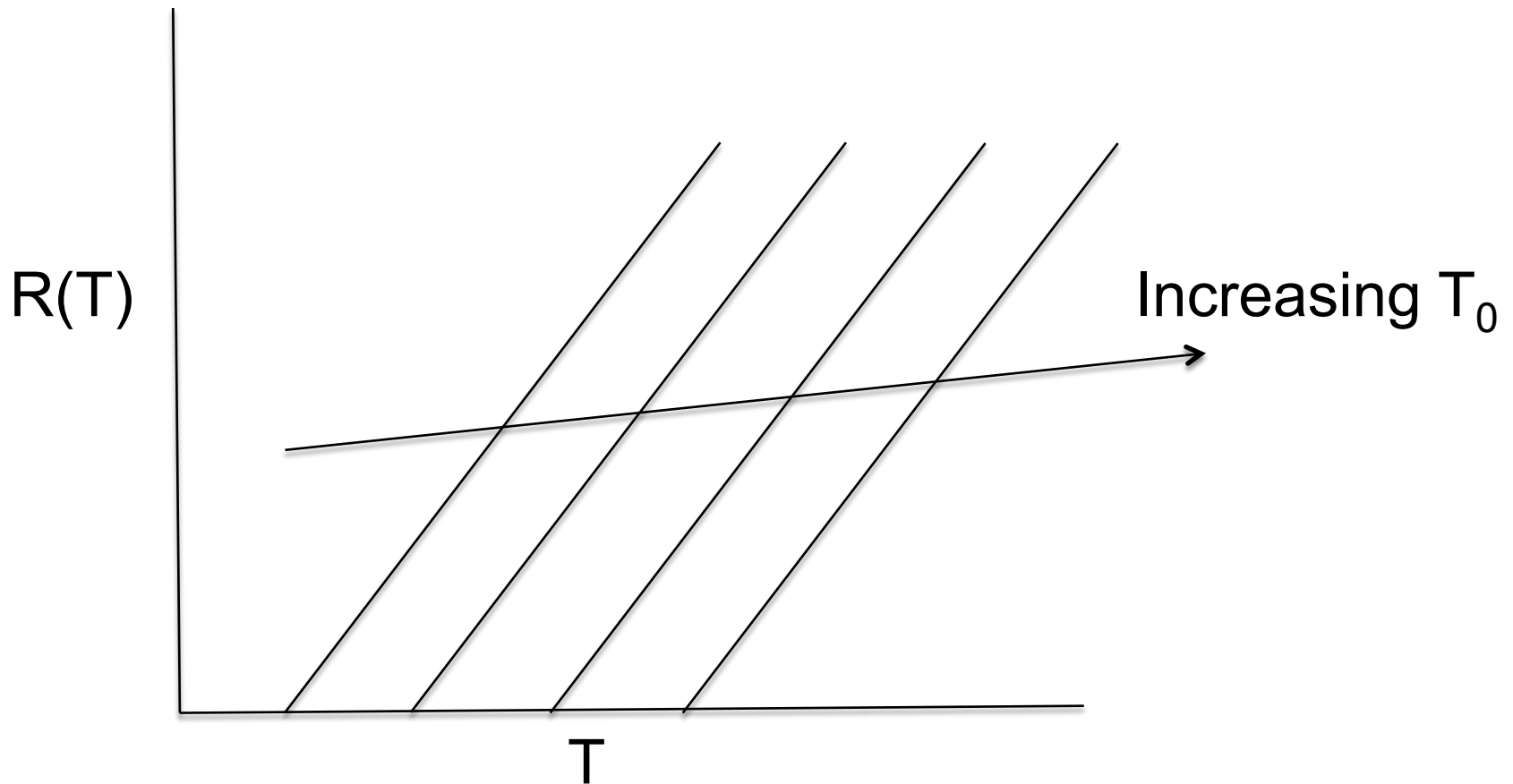
# Steady State Energy Balance for CSTRs

$$\overbrace{-X \Delta H^{\circ}_{Rx}}^{G(T)} = \overbrace{C_{P0} (1 + \kappa)(T - T_C)}^{R(T)}$$

$$X = \frac{C_{P0} (1 + \kappa)(T - T_C)}{-\Delta H^{\circ}_{Rx}}$$

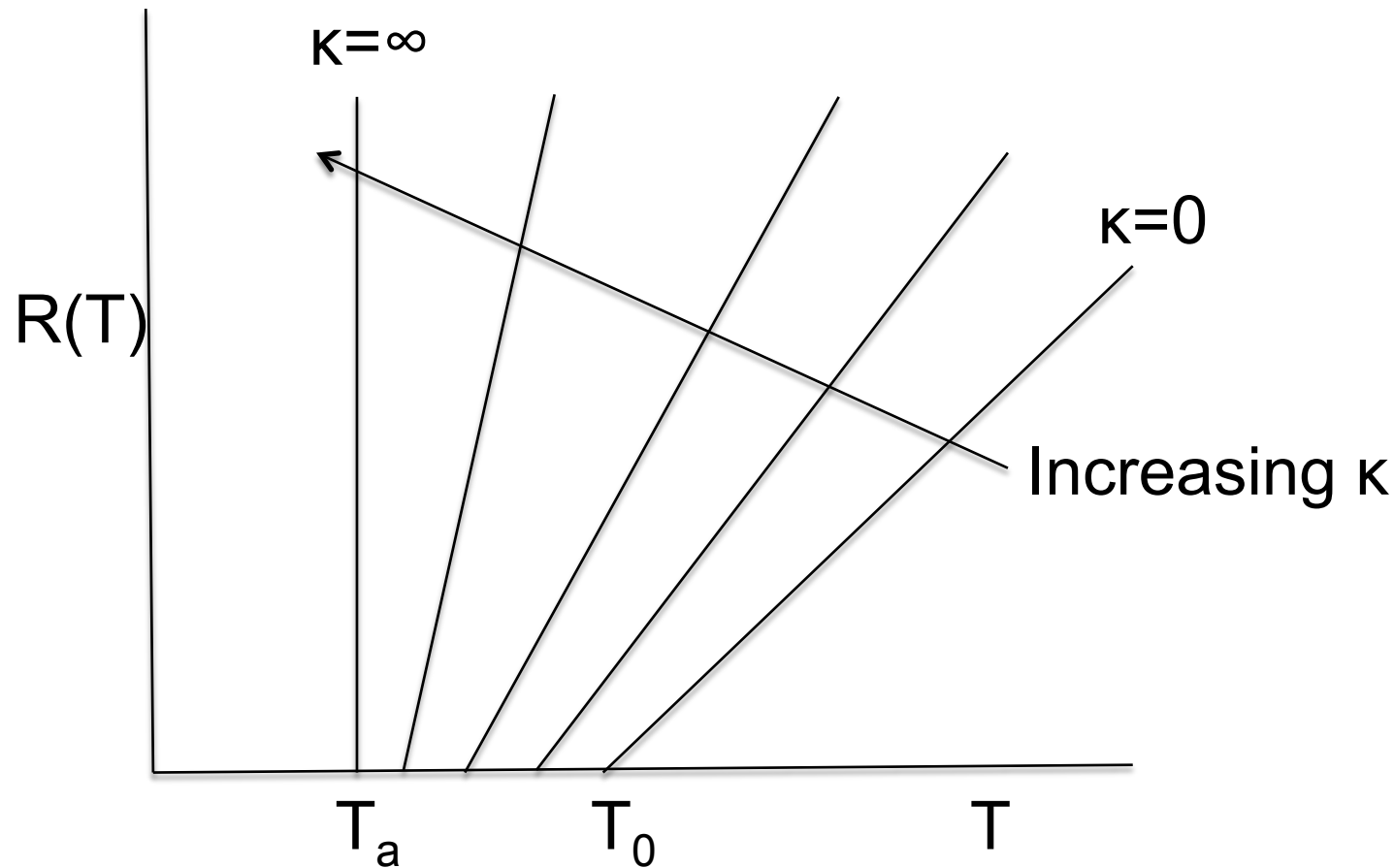
$$T = T_C + \frac{(-\Delta H^{\circ}_{Rx})(X)}{C_{P0} (1 + \kappa)}$$

# Steady State Energy Balance for CSTRs

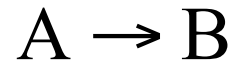


Variation of heat removal line with inlet temperature.

# Steady State Energy Balance for CSTRs



$$V = \frac{F_{A0}X}{-r_A(X, T)}$$



**1) Mole Balances:**

$$V = \frac{F_{A0}X}{-r_A}$$

**2) Rate Laws:**

$$-r_A = kC_A$$

**3) Stoichiometry:**  $C_A = C_{A0}(1 - X)$

**4) Combine:** 
$$V = \frac{F_{A0}X}{kC_{A0}(1 - X)} = \frac{C_{A0}v_0X}{kC_{A0}(1 - X)}$$

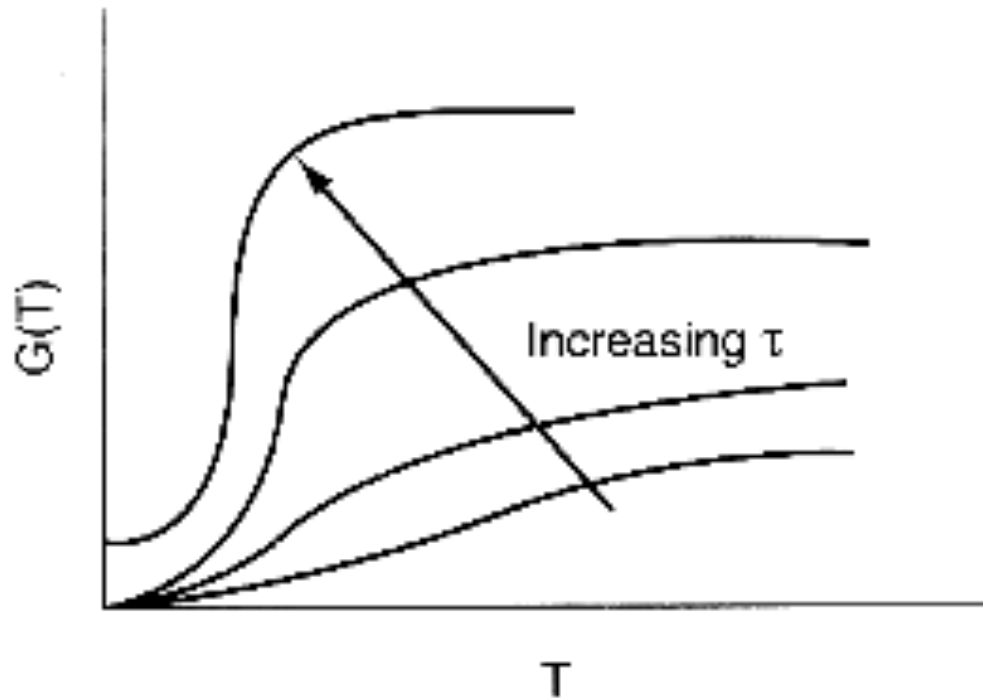
$$\tau k = \frac{X}{1 - X}$$

$$X = \frac{\tau k}{1 + \tau k} = \frac{\tau A e^{-E/RT}}{1 + A e^{-E/RT}}$$

$$G(T) = X(-\Delta H_{R_x}) = \frac{\tau A e^{-E/RT}}{1 + A e^{-E/RT}} (-\Delta H_{R_x})$$

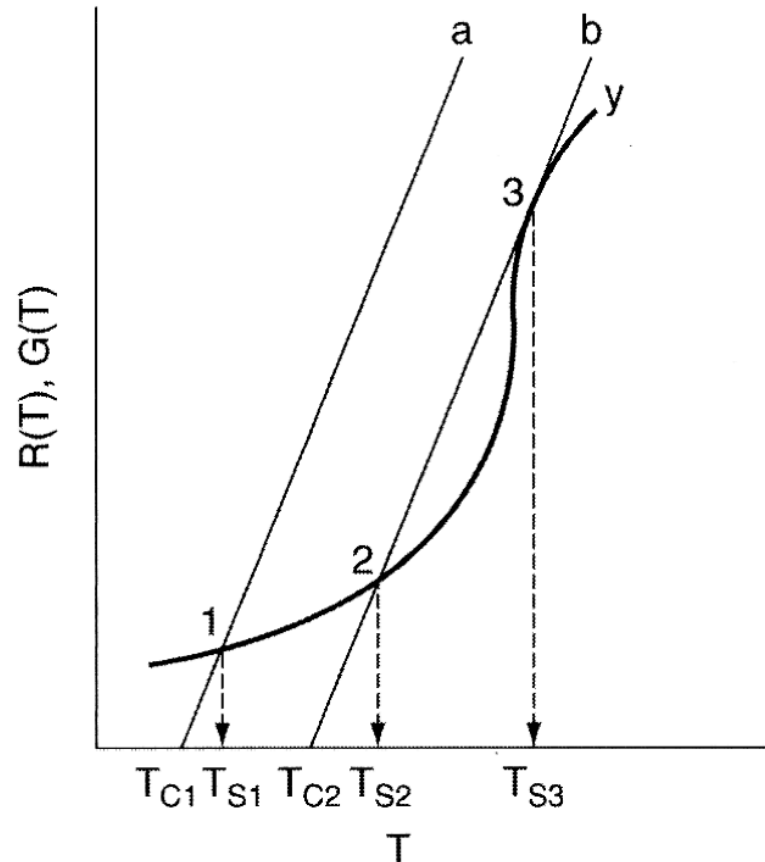


# Multiple Steady States (MSS)



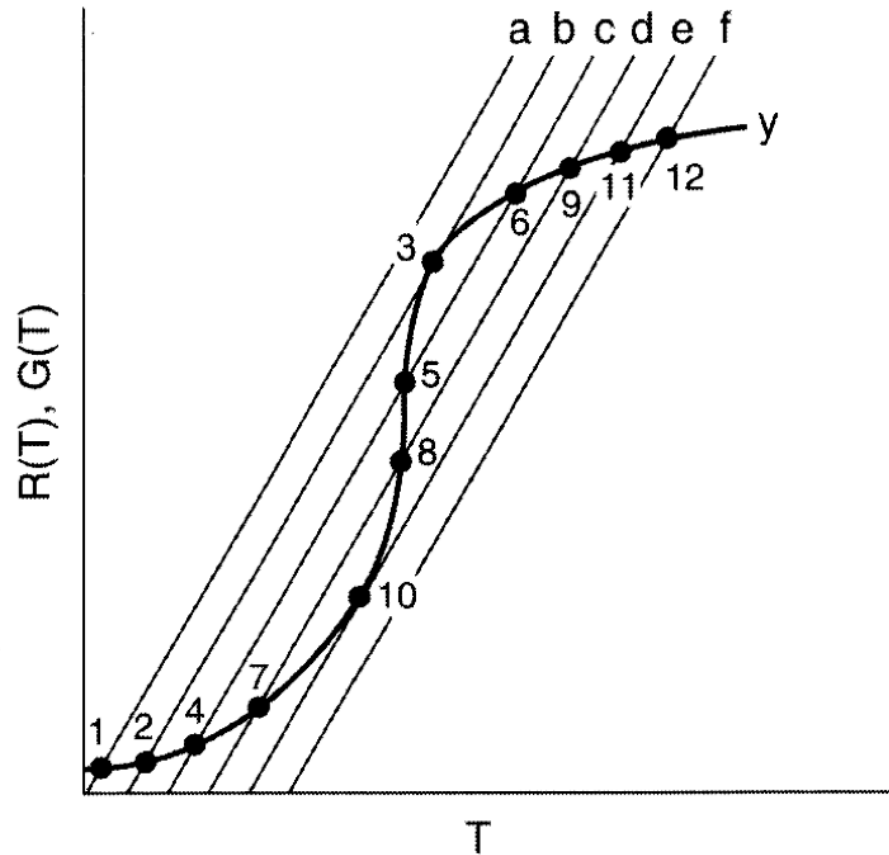
Variation of heat generation curve with space-time.

# Multiple Steady States (MSS)



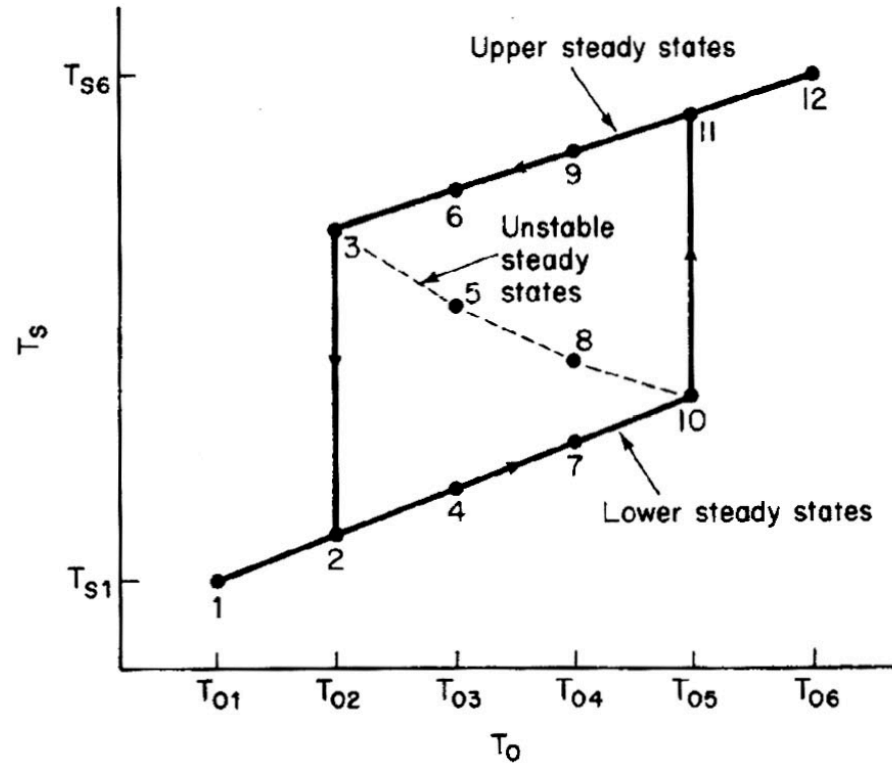
Finding Multiple Steady States with  $T_0$  varied

# Multiple Steady States (MSS)



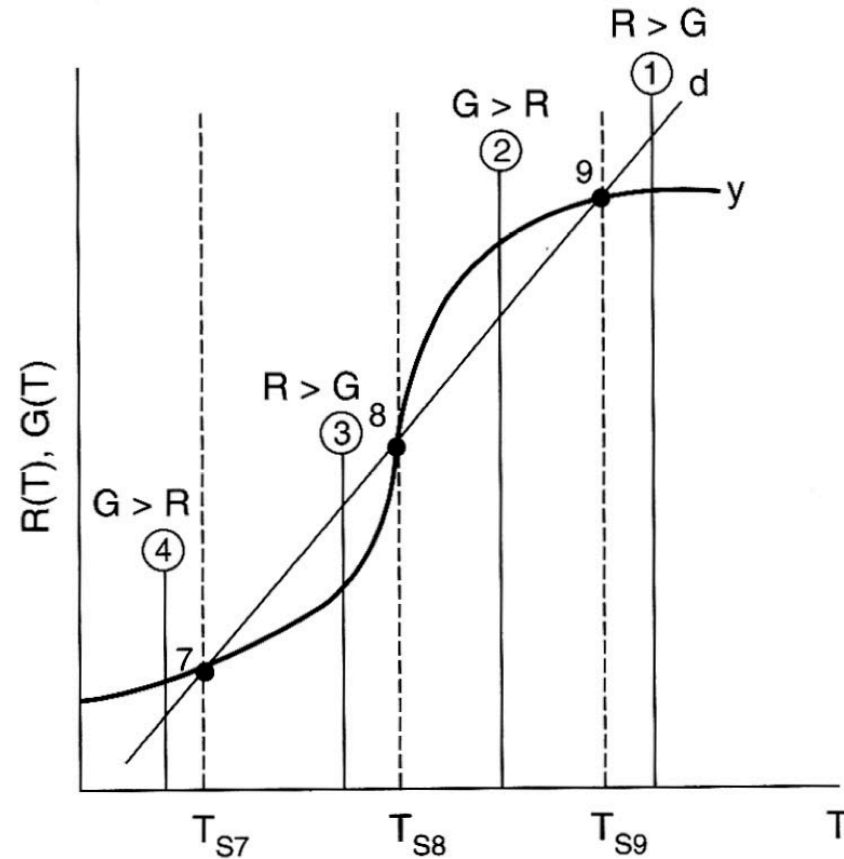
Finding Multiple Steady States with  $T_0$  varied

# Multiple Steady States (MSS)



Temperature ignition-extinction curve

# Multiple Steady States (MSS)



Stability of multiple state temperatures

# MSS - Generating G(T) and R(T)

$$\frac{dT}{dt} = 1$$

$$G(T) = X \cdot (-\Delta H_{Rx})$$

$$R = C_{P_0} \cdot (1 + \kappa) \cdot (T - T_C)$$

Need to solve for X after combining **mole balance**, **rate law**, and **stoichiometry**.

# MSS - Generating G(T) and R(T)

For a first order irreversible reaction

$$X = \frac{\tau \cdot k}{(1 + \tau \cdot k)}$$

$$k = k_1 \exp \left[ \frac{E}{R} \left( \frac{1}{T_1} - \frac{1}{T} \right) \right]$$

## Parameters

$\tau$ ,  $(-\Delta H_{RX})$ ,  $k_1$ ,  $E$ ,  $R$ ,  $T_1$ ,  $T_C$ ,  $\kappa$ ,  $C_{P_0}$

Then plot G and R as a function of T.

# End of Web Lecture 23

## Class Lecture 19