Lecture 9

Chemical Reaction Engineering (CRE) is the field that studies the rates and mechanisms of chemical reactions and the design of the reactors in which they take place.

Lecture 9 – Thursday

Balances in terms of molar flow rates

Block 1: Mole Balances

Balance Equation on Every Species

Block 2: Rate Laws

Relative Rates Transport Laws

- Block 3: Stoichiometry
- Block 4: Combine

• Membrane Reactors:

Used for thermodynamically limited reactions

Review Lecture 1

Reactor Mole Balances Summary

The GMBE applied to the four major reactor types (and the general reaction $A \rightarrow B$)



 $A + 2B \xrightarrow{\longrightarrow} C$ Mole Balance 1 Write mole balance on each species.[†] e.g., $\frac{dF_{\rm A}}{dV} = r_{\rm A}$, $\frac{dF_{\rm B}}{dV} = r_{\rm B}$, $\frac{dF_{\rm C}}{dV} = r_{\rm C}$ 2 Write rate law in terms of concentration. Rate Law e.g., $-r_{\rm A} = k_{\rm A} \left(C_{\rm A} C_{\rm B}^2 - \frac{C_{\rm C}}{K_{\rm C}} \right)$ **Relative Rates** (3) Relate the rates of reaction of each species to one another. $\frac{-r_{\rm A}}{1} = \frac{-r_{\rm B}}{2} = \frac{r_{\rm C}}{1}$ e.g., $r_{\rm B} = 2r_{\rm A}$, $r_{\rm C} = -r_{\rm A}$ Stoichiometry (4) (a) Write the concentrations in terms of molar flow rates for isothermal gas-phase reactions. e.g., $C_{\rm A} = C_{\rm T0} \frac{F_{\rm A}}{F_{\rm T}} \frac{P}{P_0}, \ C_{\rm B} = C_{\rm T0} \frac{F_{\rm B}}{F_{\rm T}} \frac{P}{P_0}$ with $F_{\rm T} = F_{\rm A} + F_{\rm B} + F_{\rm C}$ (b) For *liquid-phase* reactions, use concentration, e.g., $C_{\rm A}$, $C_{\rm B}$ Pressure Drop **(5)** Write the *gas-phase* pressure drop term in terms of molar flow rates. $\frac{dy}{dW} = -\frac{\alpha}{2y} \frac{F_{\rm T}}{F_{\rm To}}$, with $y = \frac{P}{P_0}$ Combine (6) Use an ODE solver or a nonlinear equation solver (e.g., Polymath) to combine Steps ① through ⑤ to solve for, for example, the profiles of molar flow rates, concentration, and pressure. [†] For PBR, use $\frac{dF_A}{dW} = r_A$, $\frac{dF_B}{dW} = r_B$, $\frac{dF_C}{dW} = r_C$.

Membrane reactors can be used to achieve conversions greater than the original equilibrium value. These higher conversions are the result of *Le Chatelier's principle*; you can remove the reaction products and drive the reaction to the right.

To accomplish this, a membrane that is permeable to that reaction product, but impermeable to all other species, is placed around the reacting mixture.

Dehydrogenation Reaction:

 $C_3H_8 \leftrightarrow H_2 + C_3H_6 \qquad A \leftrightarrow B + C$

Thermodynamically Limited:

exothermic





Cross section of IMRCF



Cross section of CRM

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Membrane Reactors



Schematic of IMRCF for mole balance



Membrane Reactors Mole Balance on Species A:

Species A:

 $\ln - \text{out + generation} = 0$ $F_A \Big|_V - F_A \Big|_{V+\Delta V} + r_A \Delta V = 0$

$$\frac{dF_A}{dV} = r_A$$

Membrane Reactors Mole Balance on Species B:

Species B: In – out – out membrane + generation = 0

$$F_B\Big|_V - F_B\Big|_{V+\Delta V} - R_B\Delta V + r_B\Delta V = 0$$

$$\frac{dF_B}{dV} = (r_B - R_B)$$

$$R_{B} = \frac{\text{moles of B through sides}}{\text{volume of reactor}}$$

$$W_B = k'_C (C_B - C_{BS}) = \frac{\text{molar flow rate through membrane}}{\text{surface area of membrane}} \left[\frac{mol}{m^2 \cdot s} \right]$$

$$a = \frac{\text{membrane surface area}}{\text{reactor volume}} = \frac{\pi DL}{\frac{\pi D^2}{4}L} = \frac{4}{D} \quad \left[\frac{m^2}{m^3}\right]$$

$$R_B = W_B a = k_C a \left[C_B - C_{BS} \right]$$

$$k_{C} = k_{C}a$$

$$R_{B} = k_{C}[C_{B} - C_{BS}] \quad \left[\frac{mol}{m^{3} \cdot s}\right]$$

Neglected most of the time

Mole Balances:

(1)
$$\frac{dF_A}{dV} = r_A$$

(2)
$$\frac{dF_B}{dV} = r_B - R_B$$

(3)
$$\frac{dF_C}{dV} = r_C$$

Rate Law:

$$(4) \quad r_A = -k \left[C_A - \frac{C_B C_C}{K_C} \right]$$

Membrane Reactors **Relative Rates:** $\frac{-r_A}{1} = \frac{r_B}{1} = \frac{r_C}{1}$ $(5) \quad r_{A} = -r_{B}, \quad r_{A} = -r_{C}$ **Net Rates: Transport Law:** (6) $R_B = k_C C_B$ **Stoichiometry:** (7) $C_A = C_{T0} \frac{F_A}{F_T}$ (isothermal, isobaric) $(8) \quad C_B = C_{T0} \frac{F_B}{F_T}$ $(9) \quad C_C = C_{T0} \frac{F_C}{F_T}$ (10) $F_T = F_A + F_B + F_C$ **Parameters:** $C_{\tau O} = 0.2$, $F_{AO} = 5$, k = 4, $K_C = 0.0004$, $k_C = 8$

<u>Example</u>: The following reaction is to be carried out isothermally in a membrane reactor with no pressure drop. The membrane is permeable to product C, but impermeable to all other species.



For membrane reactors, we cannot use conversion. We have to work in terms of the molar flow rates F_A , F_B , F_C .



Rate Law:

$$-r_A' = k_A \left[C_A - \frac{C_B C_C^3}{K_C} \right]$$

Relative Rates:

$$\frac{r_A'}{-1} = \frac{r_B'}{1} = \frac{r_C'}{3}$$

Net Rates:

$$r_B' = -r_A'$$

$$r_{C}' = -3r_{A}'$$

Stoichiometry: Isothermal, no Pressure Drop



 $F_T = F_A + F_B + F_C$

Combine: - Use Polymath

Parameters:
$$C_{T0} = 0.2 \frac{mol}{dm^3}$$
 $F_{A0} = 10 \frac{mol}{s}$
 $k_A = 10 \frac{dm^3}{kg \ cat \ s}$ $k_C = 0.5 \frac{dm^3}{kg \ cat \ s}$
 $K_C = 200 \frac{mol^2}{dm^6}$



End of Lecture 9